# Matrix formulation of Ritz's method, beams subjected to bending

### PROBLEM 3.1



In-plane beam with spring support and line load.

The linear elastic built-in beam with circular cross section is supported by a spring and loaded by p. We apply the approximate method of Ritz to calculate the displacement function.

- a. Calculate the deflection and angle of rotation function of the beam using MATHEMATICA. Apply  $0^{th} 6^{th}$  approximations. Record the displacement at cross section B and plot the  $v_B N_{appr}$  relationship.
- b. Plot the deformed shape using the 6<sup>th</sup> approximation function. Calculate and plot the beam diagrams (shear force and bending moment) using the 6<sup>th</sup> approximation function.

*Data:* L = 1.2 m d = 46 mm E = 200 GPa  $s = 2 \cdot 10^5 \text{ N/m}$  p = 750 N/m

The potential energy of the system is:

$$U < v >= \frac{1}{2} \int_{0}^{l} I_{z} E v^{"^{2}} dx + \frac{1}{2} s v^{2}(L) - \int_{0}^{l} (-p) v(x) dx,$$

the kinematic B.C.s are (built-in end):

v(0) = 0, v'(0) = 0.

the simplest function satisfying these conditions is  $(\omega(x))$ :

$$w(x)=x^2,$$

and the displacement function of the beam is:

$$v(x) = x^{2}(a_{0} + a_{1}x + a_{2}x^{2} + \dots ) = \underline{B}^{T}\underline{A}.$$

# **MATHEMATICA solution**

**Definition of the geometrical and material properties (units are in SI)** p=750;L=1.2;d=0.046;Iz=d^4\*Pi/64;Ex=200\*10^9;s=2\*10^5; omega=x^2;

**Definition of the number of approximation** Nappr=0;

### Calculation of B<sup>T</sup>, the 1<sup>st</sup> and 2<sup>nd</sup> derivative of B

Bt=Transpose[B]; dB=D[B,x]; ddB=D[B,{x,2}]; ddBt=Transpose[ddB];

### Construction of the stiffness matrix and the vector of external forces

 $S=Integrate[Iz*Ex*ddB.ddBt, \{x,0,L\}]+s*(B.Bt)/.x->L;$  $Q=Integrate[-p*B, \{x,0,L\}]$ 

## Calculation of the vector of unknown coefficients

A=Inverse[S].Q;

### **Deflection and angle of rotation function**

v[x\_]=Transpose[B].A; phi[x\_]=D[v[x],x];

# Calculate the deflection and the rotation at cross section B

vb=v[L] phib=phi[L]

### **Convergence**

convvb={}; convphib= {};

Repeat this procedure until the 6<sup>th</sup> approximation, run the worksheet again, increase "Nappr" at each step, put the results into the table.

### Plot the data

ListPlot[convvb] ListPlot[convphib]

### Animation of deflection and angle of rotation functions

$$\label{eq:animate} \begin{split} &Animate[Plot[t*v[x], \{x, 0, L\}, PlotRange-> \{All, \{0, -0.001222\}\}, AspectRatio->0.2], \{t, 0, 1\}] \\ &Animate[Plot[t*phi[x], \{x, 0, L\}, PlotRange-> \{All, \{0, -0.0015\}\}, AspectRatio->0.2], \{t, 0, 1\}] \end{split}$$

### Beam diagrams, bending moment and shear force, animation

$$\label{eq:mbs} \begin{split} Mb[x_] = & Iz^*Ex^*D[v[x], \{x,2\}]; \\ V[x_] = & -D[Mb[x], x] \\ Animate[Plot[t^*Mb[x], \{x,0,L\}, PlotRange-> \{All, \{-250,40\}\}, AspectRatio->0.2], \{t,0,1\}] \\ Animate[Plot[t^*V[x], \{x,0,L\}, PlotRange-> \{All, \{-670,250\}\}, AspectRatio->0.2], \{t,0,1\}] \end{split}$$

*Results: (6th approximation):*  $V_A = 655.8 \text{ N}, M_A = 246.9 \text{ Nm}, V_B = -244.3 \text{ N}, M_B = 0 \text{ Nm},$ 

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In-plane beam with piecewise continuous cross section.

- a. Calculate the deflection and angle of rotation function of the beam. Apply  $0^{th} 8^{th}$  approximations. Record the displacement at cross section B and plot the  $v_B N_{appr}$  relationship.
- b. Plot the deformed shape using the  $8^{th}$  approximation function. Calculate and plot the beam diagrams (shear force and bending moment) using the  $8^{th}$  approximation function.
- Data:a = 1 mb = 0.8 m $d_1 = 60 \text{ mm}$  $d_2 = 46 \text{ mm}$  $E_1 = 210 \text{ GPa}$  $E_2 = 190 \text{ GPa}$  $s = 2 \cdot 10^5 \text{ N/m}$ p = 800 N/mF = 1000 NF = 1000 NF = 1000 N $s = 2 \cdot 10^5 \text{ N/m}$ p = 800 N/m

The potential energy of the system is:

$$U < v >= \frac{1}{2} \int_{0}^{a} I_{z1} E_{1} v''^{2} dx + \frac{1}{2} \int_{a}^{a+b} I_{z2} E_{2} v''^{2} dx + \frac{1}{2} sv^{2}(L) - \int_{0}^{a} (-p)v(x) dx - (-F)v(a+b/2)$$

*Hint: Modify the worksheet of Problem 3.1....Results:*  $v_B = -2.733 \text{ mm}, \quad \varphi_B = -0.000169 \text{ rad}$